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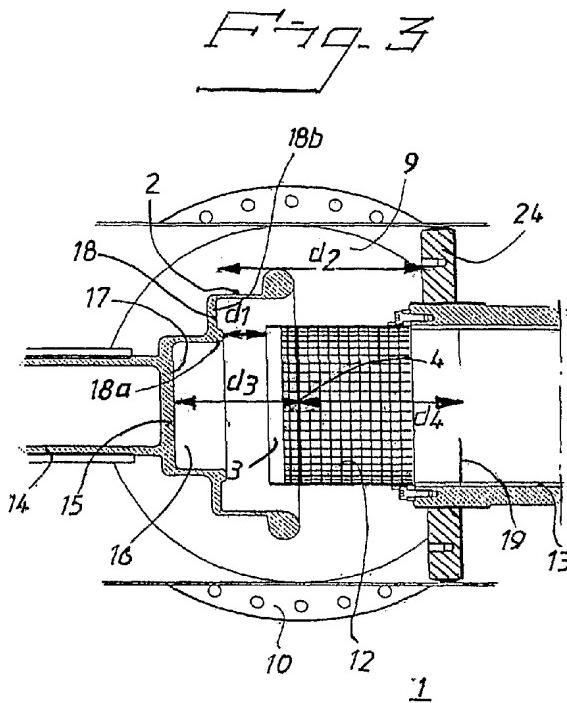
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**(54) Title: DEVICE FOR THE GENERATION OF MICROWAVES**



**(57) Abstract:** The invention relates to a device for the generation of microwaves, comprising a virtual cathode oscillator (1) in coaxial construction having an outer substantially cylindrical tube constituting a cathode (2) and connected to a transmission conductor (14) for feeding the cathode (2) with voltage pulses, as well as an inner substantially cylindrical tube, at least partially transparent for electrons, constituting an anode (3) and connected to a wave guide (13) for the discharge of microwave radiation generated by the formation of a virtual cathode (4) inside a region enclosed by the anode. The device comprises an electrically conductive structure in the form of a reflector (19) disposed adjacent to the anode (3). The cathode (2) comprises a substantially rotationally symmetric, electrically conductive body (15) having a cavity (16). By configuring the cavity (16) in the body (15) of the cathode with a first, lesser depth to that boundary surface (18) of the body which is directly in front of the peripheral part of the closure of the anode (3) against the cathode, and a second, greater depth to the boundary surface (17) of the body directly in front of the central part of the closure of the anode (3) against the cathode, a device for the generation of microwaves is produced, which has higher efficiency and high peak power.

**Case 1101**

## Device for the generation of microwaves

5 The present invention relates to a device for the generation of microwaves, comprising a virtual cathode oscillator in coaxial construction having an outer substantially cylindrical tube constituting a cathode and connected to a transmission conductor for feeding  
10 the cathode with voltage pulses, as well as an inner substantially cylindrical tube, at least partially transparent for electrons, constituting an anode and connected to a wave guide for the discharge of microwave radiation generated by the formation of a  
15 virtual cathode inside a region enclosed by the anode, wherein an electrically conductive structure in the form of a reflector is disposed adjacent to the anode, and wherein the cathode comprises a substantially rotationally symmetric, electrically conductive body  
20 having a cavity.

A device according to the first paragraph is essentially previously known through "Microwave frequency determination mechanisms in a coaxial  
25 vircator", Xupeng Chen et al, IEEE Transactions on Plasma Science, Vol. 32, Issue 5, Oct. 2004, pp. 1799-1804.

Microwave generators of this kind can, inter alia, be  
30 used to disable electronics by virtue of the high peak powers which can be briefly generated, or to generate pulses in systems which require high-power pulses for a short period.

35 A general problem with virtual cathode oscillators, often termed "vircators" in English, is that they are low in efficiency. There are therefore strong requirements to be able to improve the efficiency of the device. Moreover, it may be valuable to be able to

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increase the peak power and peak power efficiency of the device.

One object of the present invention is to provide a  
5 device for the generation of microwaves with improved efficiency. Another object is to improve the peak power of the device. Since the virtual cathode oscillator, the vircator, is primarily used to create high-power microwave radiation, the peak power efficiency,  
10 specifically, is a very important parameter.

The objects of the invention are achieved by a device for the generation of microwaves according to the first paragraph, characterized in that the cavity in the body 15 of the cathode is configured with a first, lesser depth to that boundary surface of the body which is directly in front of the peripheral part of the closure of the anode against the cathode, and a second, greater depth to that boundary surface of the body which is directly 20 in front of the central part of the closure of the anode against the cathode.

Through the introduction of a substantially rotationally symmetric, electrically conductive body 25 with divergent depth relative to the closure of the anode against the cathode end, a favourable interaction between anode and cathode has been realized, resulting in increased efficiency and enhanced peak power efficiency. The increase in efficiency and peak power 30 has been able to be verified by experiments and simulations.

Especially favourable improvements in efficiency and peak power are obtained if the body of the cathode is 35 dimensioned with cavity and arrangement in relation to anode, reflectors and stop walls such that, according to a preferred embodiment, the closure of the device against the cathode is disposed at a distance to the boundary surface for the first, lesser depth of the

body, which distance is substantially equal to an odd multiple of the quarter-wavelength for the microwaves to be generated. In particular, a compact construction is offered where the closure of the anode against the 5 cathode is disposed at a distance to the boundary surface for the first, lesser depth of the body, which distance is substantially equal to a quarter-wavelength for the microwaves to be generated. By choosing the smallest odd multiple of a quarter-wavelength, other 10 distances which depend on this distance for their dimensioning can be made short, resulting in a compact device.

Further favourable improvements can be obtained if, 15 according to another preferred embodiment, the boundary surface for the second, greater depth of the body is arranged at a distance to the formed virtual cathode in the anode, which distance substantially corresponds to an odd multiple of the quarter-wavelength for the 20 microwaves to be generated and is greater than a quarter-wavelength.

In addition, according to another preferred embodiment, the reflector can be disposed in the tube of the anode, 25 which tube is at least partially transparent for electrons, transversely to the longitudinal direction of the tube at a distance from the virtual cathode formed in the anode, which distance substantially corresponds to an odd multiple of the quarter-wavelength for the 30 microwaves to be generated.

According to yet another preferred embodiment, an electrically conductive stop wall is disposed on the outer side of the tube of the anode, which tube is at 35 least partially transparent for electrons, transversely to the longitudinal direction of the tube at a distance which is substantially equal to an odd multiple of the quarter-wavelength for the microwaves to be generated and is greater than a quarter-wavelength from the

boundary surface of the cathode for the first, lesser depth.

Advantageously, the boundary surface of the body for  
5 the lesser depth is configured with a somewhat  
increasing depth in that part of the boundary surface  
which lies at the radially greatest distance from the  
rotational axis of the body. This slight increase in  
the depression at the radially greatest distance  
10 contributes to the favourable realization of distances  
specified for the device, with respect to multiples of  
odd quarter-wavelengths.

A suitable reflector disposed adjacent to the anode  
15 comprises one or more electrically conductive surfaces  
for partially filling a cross section of the tubular  
anode. It is especially proposed that the electrically  
conductive surfaces of the reflector are constituted by  
metal strips. By virtue of the proposed configuration  
20 of the reflector, which can be structurally simple, a  
reflector with suitable balance between reflected and  
transmitted microwaves is produced. According to a  
proposed embodiment, the reflector is here configured  
25 with two opposite circle sectors forming electrically  
conductive surfaces. According to another embodiment,  
the reflector is configured as a central strip forming  
an electrically conductive surface. According to a  
further proposed embodiment, the reflector is  
30 configured with two strip sections separated in the  
centre of the reflector and forming an electrically  
conductive surface.

In an expedient embodiment, the electrically conductive  
body of the cathode is proposed to consist  
35 substantially of aluminium. The proposed material has  
the advantage of low weight and is relatively easy to  
machine, for example by turning.

For feeding of the cathode of the device, a high-voltage generator is expediently connected to the transmission conductor of the cathode. In addition, the wave guide for discharge of the microwave radiation is  
5 connected to an aerial. The aerial, it is proposed, can be a horn aerial.

The invention will be described in greater detail below  
in exemplified form with reference to the appended  
10 drawings, in which:

Figure 1 shows schematically an example of a known coaxial virtual cathode oscillator forming part of a device for the generation of microwaves,  
15

Figure 2 shows schematically in sectional view an example of a coaxial virtual cathode oscillator according to the invention, forming part of a device for the generation of microwaves,  
20

Figure 3 shows a more detailed example in sectional view of a coaxial virtual cathode oscillator according to the invention, forming part of a device for the generation of microwaves,  
25

Figure 4 shows schematically in block form a complete device for the generation of microwaves, comprising a coaxial virtual cathode oscillator according to the invention,  
30

Figures 5a, 5b and 5c show schematically three examples of the configuration of a reflector which can form part of the coaxial virtual cathode oscillator shown in Figure 2 or 3.  
35

The known coaxial virtual cathode oscillator 1 which is shown in highly schematic representation in Figure 1 comprises a cathode 2 in the form of an outer cylindrical tube and an anode 3 in the form of an inner

cylindrical tube. The cathode oscillator is of a very simple geometric design and is based on the fact that a so-called virtual cathode 4 is formed inside the anode under certain conditions.

5

Figure 2 shows somewhat less schematically in longitudinal cross section a modification of the known coaxial virtual cathode oscillator for improving the efficiency and enhancing the peak power. According to 10 this embodiment, the cathode 2 is provided with a rotationally symmetric body 15 having a cavity 16 and the shape of the body can be most closely likened to the shape of a cup. The cavity 16 is configured such that it has a greater depth in the central parts of the 15 body having a boundary surface 17, and a lesser depth in the outermost part (viewed radially from the centre of the body) having a boundary surface 18. The boundary surface 18 can in turn be divided into an inner part 18a of somewhat lower depth than an outer part 18b.

20

A conductive structure in the form of a reflector 19 is disposed in the interior of the anode. Figures 5a, 5b and 5c show three examples of possible configurations of the reflector 19. The reflectors comprise 25 electrically conductive surfaces, which partially fill the cross section shaped by the tubular interior of the anode 3. According to the example in Figure 5a, the conductive surfaces form two diagonally opposing circle sectors 20, 21, symmetrically centred with respect to a 30 circle diameter 26. In Figure 5b, the electrically conductive surface is constituted by a band 22, which is symmetrically centred with respect to the circle diameter 26. In Figure 5c, the electrically conductive surface is constituted by two band sections 22a and 35 22b, which are symmetrically centred with respect to the circle diameter 26 and are separated from each other in the central part of the surrounding circle 23. In Figures 5a and 5b, the circle diameter 26 is marked by means of a dashed line. The circle 23 surrounding

the conductive surfaces can be regarded as a mount for the conductive surfaces. Alternatively, the circle can symbolize the inner circumference of the tubular anode 3, in which the conductive surfaces can be directly fastened in the cathode tube.

On the outer side of the tubular anode 3, there is disposed a stop wall 24 consisting of an electrically conductive material, such as aluminium or copper.

10

In the figure there are four different distances,  $d_1-d_4$ , marked as follows:

- $d_1$  marks the distance between the boundary surface 18a and the closure of the anode against the cathode,
- 15 -  $d_2$  marks the distance between the stop wall 24 and the boundary surface 18b,
- $d_3$  marks the distance between the boundary surface 17 and the virtual cathode 4 which is formed in the anode 3, and
- 20 -  $d_4$  marks the distance between the virtual cathode 4 and the reflector 19 disposed in the interior of the tubular anode.

The distances  $d_1$  to  $d_4$  are advantageously chosen as follows:

$$\begin{aligned} d_1 &= \lambda * n / 4, \text{ where } n = 1, 3, 5, \dots \\ d_2 &= \lambda * n / 4, \text{ where } n = 3, 5, 7, \dots \\ d_3 &= \lambda * n / 4, \text{ where } n = 3, 5, 7, \dots \\ 30 \quad d_4 &= \lambda * n / 4, \text{ where } n = 1, 3, 5, \dots \end{aligned}$$

with the secondary condition that  $d_2$  and  $d_3 > d_1$ .

The coaxial virtual cathode oscillator 1 can form part of a device for the generation of microwaves shown in Figure 4 and comprising a high-voltage generator 7 connected to the input of the cathode oscillator and an aerial 8 connected to the output of the cathode oscillator. The aerial can be a horn aerial.

The cathode oscillator with peripheral arrangements is now shown and described in greater detail with reference to Figure 3, both as regards configuration 5 and working. Reference symbols having correspondence in previously described figures have been denoted with the same reference symbols in Figure 3. According to Figure 3, the anode 3 and cathode 2 are disposed in a vacuum chamber 9 to which there is a connection 10 for a 10 vacuum pump (not shown). The anode 3 is provided with a grid 12, which is in part transparent for free, electrically charged particles. The anode 3 passes into an outbound wave guide 13, whilst the cathode 2 is fed via a transmission conductor 14.

15

The design of the cathode oscillator is based on the fact that a so-called virtual cathode is formed under certain conditions. When a voltage pulse with negative potential is applied via the transmission conductor 14 20 to the cathode 2, a highly electrical field is created between the cathode 2 and the anode 3. This results in electrons being field-emitted from the cathode material. The electrons are subsequently accelerated towards the anode structure and the majority of the 25 electrons will also pass through the anode and begin to be retarded. If certain conditions are met, a virtual cathode 4 will be formed inside the anode structure. Owing to the fact that the process is strongly non-linear, phenomena occur which result in the generation 30 of microwave radiation. The more detailed preconditions for the microwave generation are not described here, since this belongs to the sphere of competence of a person skilled in the art. Under the right preconditions, very high power is briefly generated in 35 the order of magnitude, typically, of 50-100 ns, before short-circuiting occurs. Generated microwaves leave the anode of the cathode oscillator via the wave guide 13 connected to the anode, which has substantially the same radius as the anode 3. By configuring the body 15

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with a cavity 16 and boundary surfaces 17, 18 of varying depth in interaction with the anode 3, introducing the reflector 19 and possibly the stop wall 24 and, as far as possible, applying the above-5 specified distance measurements with respect to  $d_1-d_4$ , high-power pulses can be generated with substantially improved efficiency and peak power.

The invention is not limited to the embodiments shown  
10 above by way of example, but can be subjected to modifications within the scope of the following patent claims.

## Patent claims

1. Device for the generation of microwaves,  
5 comprising a virtual cathode oscillator in coaxial construction having an outer substantially cylindrical tube constituting a cathode and connected to a transmission conductor for feeding the cathode with voltage pulses, as well as an inner substantially cylindrical tube, at least partially transparent for electrons, constituting an anode and connected to a wave guide for the discharge of microwave radiation generated by the formation of a virtual cathode inside a region enclosed by the anode, wherein an electrically  
10 conductive structure in the form of a reflector is disposed adjacent to the anode, and wherein the cathode comprises a substantially rotationally symmetric, electrically conductive body having a cavity,  
**characterized in that** the cavity in the body of the  
20 cathode is configured with a first, lesser depth to that boundary surface of the body which is directly in front of the peripheral part of the closure of the anode against the cathode, and a second, greater depth to that boundary surface of the body which is directly  
25 in front of the central part of the closure of the anode against the cathode.

2. Device according to Patent Claim 1,  
**characterized in that** the closure of the device against  
30 the cathode is disposed at a distance to the boundary surface for the first, lesser depth of the body, which distance is substantially equal to an odd multiple of the quarter-wavelength for the microwaves to be generated.

35

3. Device according to Patent Claim 2,  
**characterized in that** the closure of the anode against the cathode is disposed at a distance to the boundary surface for the first, lesser depth of the body, which

distance is substantially equal to a quarter-wavelength for the microwaves to be generated.

4. Device according to any one of the preceding  
5 patent claims, **characterized in that** the boundary surface for the second, greater depth of the body is arranged at a distance to the formed virtual cathode in the anode, which distance substantially corresponds to an odd multiple of the quarter-wavelength for the  
10 microwaves to be generated and is greater than a quarter-wavelength.

5. Device according to any one of the preceding patent claims, **characterized in that** the reflector is  
15 disposed in the tube of the anode, which tube is at least partially transparent for electrons, transversely to the longitudinal direction of the tube at a distance from the virtual cathode formed in the anode, which distance substantially corresponds to an odd multiple  
20 of the quarter-wavelength for the microwaves to be generated.

6. Device according to any one of the preceding patent claims, **characterized in that** an electrically  
25 conductive stop wall is disposed on the outer side of the tube of the anode, which tube is at least partially transparent for electrons, transversely to the longitudinal direction of the tube at a distance which is substantially equal to an odd multiple of the  
30 quarter-wavelength for the microwaves to be generated and is greater than a quarter-wavelength from the boundary surface of the cathode for the first, lesser depth.

35 7. Device according to any one of the preceding patent claims, **characterized in that** the boundary surface of the body for the lesser depth is configured with a somewhat increasing depth in that part of the

boundary surface which lies at the radially greatest distance from the rotational axis of the body.

8. Device according to any one of the preceding  
5 patent claims, **characterized in that** the reflector disposed adjacent to the anode comprises one or more electrically conductive surfaces for partially filling a cross section of the tubular anode.

10 9. Device according to Claim 8, **characterized in that** the electrically conductive surfaces of the reflector are constituted by metal strips.

15 10. Device according to any one of Patent Claims 8 or 9, **characterized in that** the reflector is here configured with two opposite circle sectors forming electrically conductive surfaces.

20 11. Device according to any one of Patent Claims 8 or 9, **characterized in that** the reflector is configured as a central strip forming an electrically conductive surface.

25 12. Device according to any one of Patent Claims 8 or 9, **characterized in that** the reflector is configured with two strip sections separated in the centre of the reflector and forming an electrically conductive surface.

30 13. Device according to any one of the preceding patent claims, **characterized in that** the electrically conductive body of the cathode consists substantially of aluminium.

35 14. Device according to any one of the preceding patent claims, **characterized in that** the transmission conductor for feeding of the cathode is connected to a high-voltage generator.

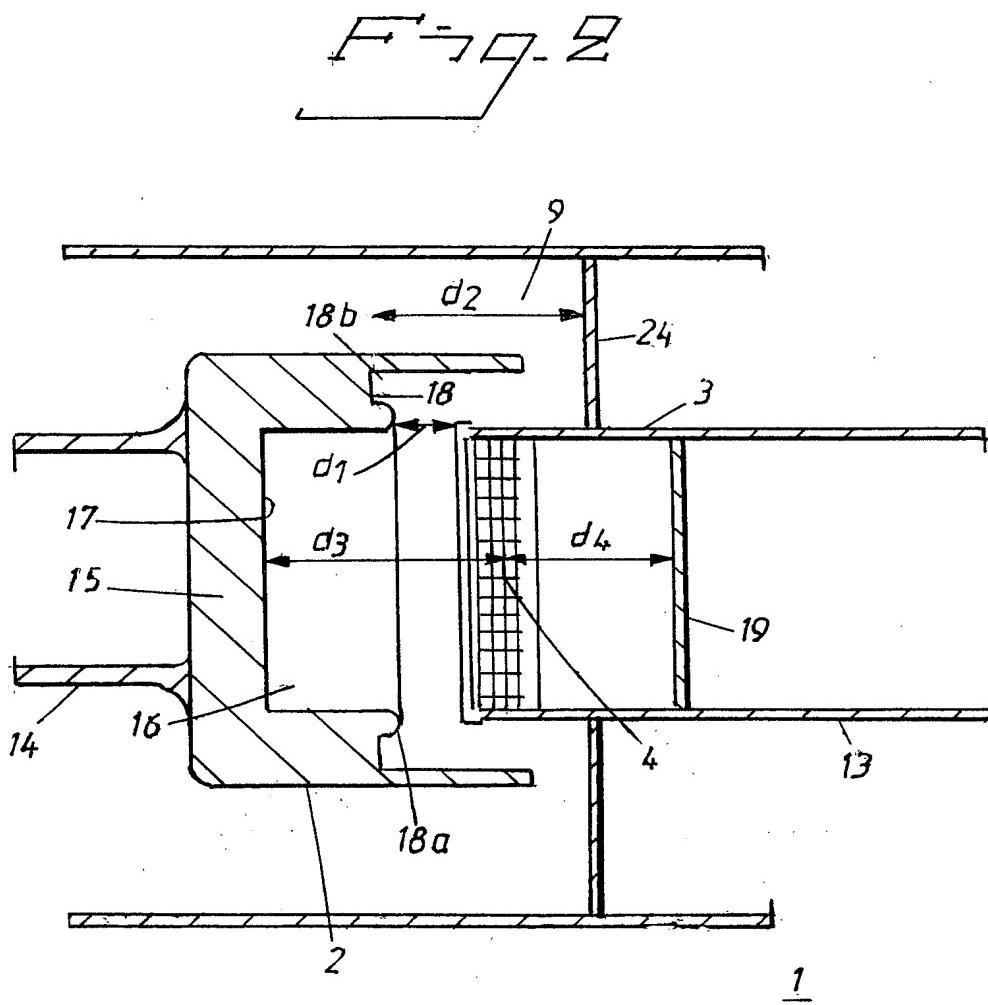
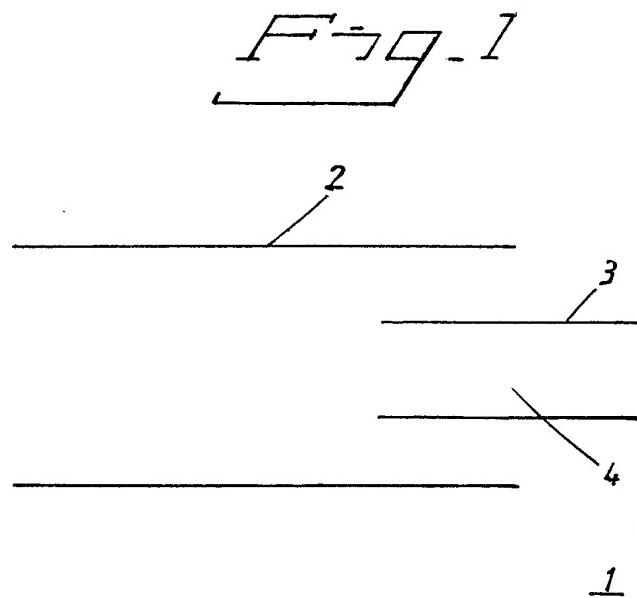
- 13 -

15. Device according to any one of the preceding patent claims, **characterized in that** the wave guide for discharge of the microwave radiation is connected to an aerial.

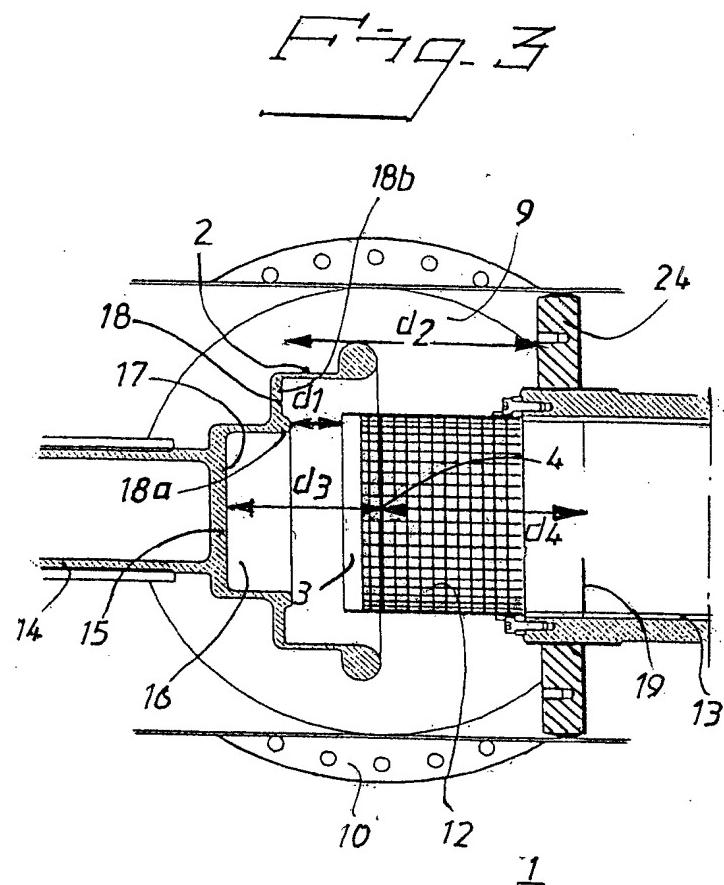
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16. Device according to Patent Claim 15, **characterized in that** the aerial is a horn aerial.

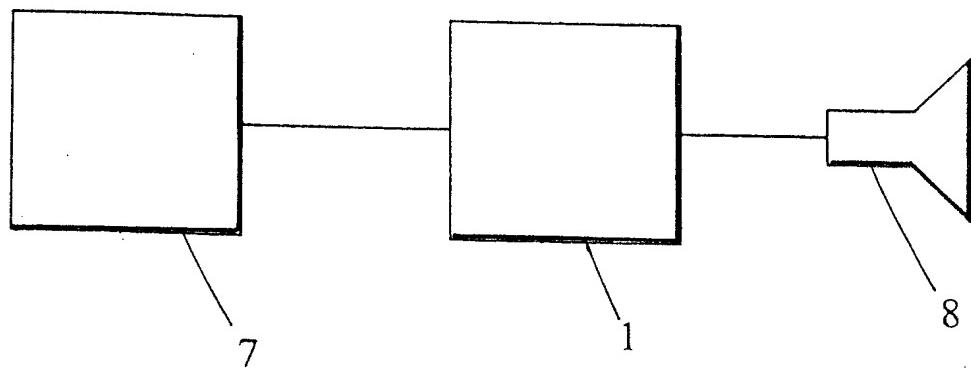
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3/3

Fig. 5a

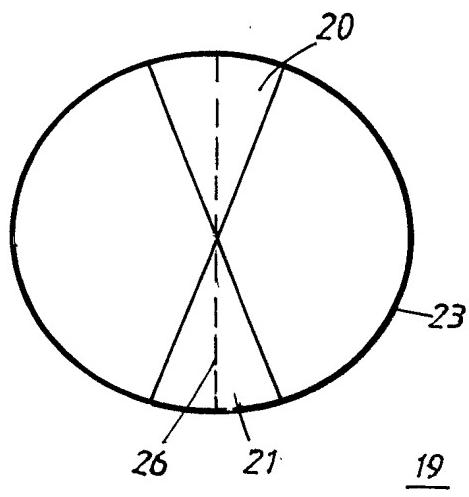


Fig. 5b

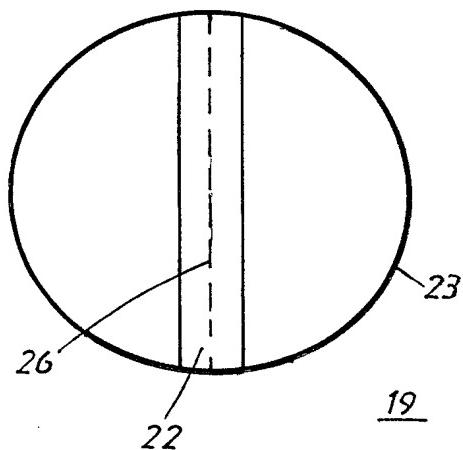
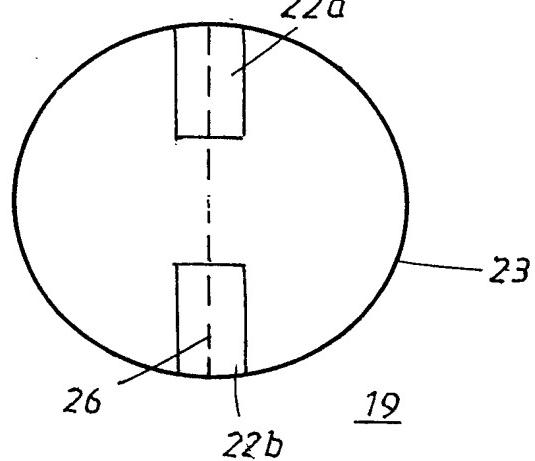
1919

Fig. 5c

22b19

**INTERNATIONAL SEARCH REPORT**

International application No.

PCT/SE2009/000191

**A. CLASSIFICATION OF SUBJECT MATTER**

**IPC: see extra sheet**

According to International Patent Classification (IPC) or to both national classification and IPC

**B. FIELDS SEARCHED**

Minimum documentation searched (classification system followed by classification symbols)

**IPC: H01J**

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

**SE,DK,FI,NO classes as above**

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

**EPO-INTERNAL, WPI DATA, PAJ**

**C. DOCUMENTS CONSIDERED TO BE RELEVANT**

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	<p><b>DT - Journal Article</b>  <b>TI - Microwave Frequency Determination Mechanisms in a Coaxial Vircator</b>  <b>AU - Chen X; Choi E H; Dickens J; Hatfield L L; Kristiansen M; Mankowski J</b>  <b>PUB - IEEE TRANSACTIONS ON PLASMA SCIENCE, - 20041001</b>  <b>- IEEE SERVICE CENTER, PISCATAWAY, NJ, US</b>  <b>IRN - ISSN 0093-3813, VOL - 32, NR - 5,</b>  <b>PG - 1799 - 1804; whole document; figure 1</b></p> <p style="text-align: center;">---</p>	1-16

Further documents are listed in the continuation of Box C.

See patent family annex.

* Special categories of cited documents:	
"A"	document defining the general state of the art which is not considered to be of particular relevance
"E"	earlier application or patent but published on or after the international filing date
"L"	document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)
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"P"	document published prior to the international filing date but later than the priority date claimed
"T"	later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
"X"	document of particular relevance: the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
"Y"	document of particular relevance: the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art
"&"	document member of the same patent family

Date of the actual completion of the international search

6 August 2009

Date of mailing of the international search report

07-08-2009

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## INTERNATIONAL SEARCH REPORT

International application No. PCT/SE2009/000191
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## C (Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	<p><b>DT - Journal Article</b>  <b>"Influence of Anode-Cathode Gap Distance on Output Characteristics of High-Power Microwave From Coaxial Virtual Cathode Oscillator"</b>, Choi E H et al; PUB - IEEE TRANSACTIONS ON PLASMA SCIENCE, - 20050801, - IEEE SERVICE CENTER, PISCATAWAY, NJ, US, IRN - ISSN 0093-3813; VOL - 33, NR - 4, PG. - 1353 - 1357  Abstract  --</p>	1-16
A	<p>Xiaodong Chen; Toh, W.K.; Lindsay, P.A., 'Physics of the interaction Process in a typical coaxial virtual cathode oscillator based on computer modeling using MAGIC,' Plasma Science, IEEE Transactions on , vol.32, no.3, pp. 1191-1199, June 2004  URL:  <a href="http://ieeexplore.ieee.org/stamp/stamp.jsp?arnumber=1321281&amp;isnumber=29266">http://ieeexplore.ieee.org/stamp/stamp.jsp?arnumber=1321281&amp;isnumber=29266</a>  Figure 2,9; Abstract  --</p>	1-16
A	<p>Hao Shao; Guozhi Liu; Zhimin Song; Yajun Fan; Xiaoxin Song, 'Numerical simulation studies of coaxial vircators,' High-Power Particle Beams, 1998. BEAMS '98. Proceedings of the 12th International Conference on , vol.2, no., pp.792-795 vol.2, 1998  URL:  <a href="http://ieeexplore.ieee.org/stamp/stamp.jsp?arnumber=816972&amp;isnumber=17692">http://ieeexplore.ieee.org/stamp/stamp.jsp?arnumber=816972&amp;isnumber=17692</a>  Whole document  --</p>	1-16
A	<p>Cecilia Möller, Tomas Hurtig, Anders Larsson and Sten E. Nyholm: 'Numerical Simulation of Direct Excitation of the TE11 Mode in a Coaxial Vircator'. IEEJ Trans. FM, Vol. 127, No. 11, pp.687-692 (2007)  doi: 10.1541/ieejfms.127.687  JOI JSTJSTAGE/ieejfms/127.687  Sammandrag  --  -----</p>	1-16

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**PUBN-DATE:** November 12, 2009

**INVENTOR-INFORMATION:**

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KARLSSON MAGNUS	SE

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**INT-CL (IPC):** H01J025/02

**EUR-CL (EPC):** H01J025/02

**ABSTRACT:**

CHG DATE=20091113 STATUS=N>The invention relates to a

device for the generation of microwaves, comprising a virtual cathode oscillator (1) in coaxial construction having an outer substantially cylindrical tube constituting a cathode (2) and connected to a transmission conductor (14) for feeding the cathode (2) with voltage pulses, as well as an inner substantially cylindrical tube, at least partially transparent for electrons, constituting an anode (3) and connected to a wave guide (13) for the discharge of microwave radiation generated by the formation of a virtual cathode (4) inside a region enclosed by the anode. The device comprises an electrically conductive structure in the form of a reflector (19) disposed adjacent to the anode (3). The cathode (2) comprises a substantially rotationally symmetric, electrically conductive body (15) having a cavity (16). By configuring the cavity (16) in the body (15) of the cathode with a first, lesser depth to that boundary surface (18) of the body which is directly in front of the peripheral part of the closure of the anode (3) against the cathode, and a second, greater depth to the boundary surface (17) of the body directly in front of the central part of the closure of the anode (3) against the cathode, a device for the generation of microwaves is produced, which has higher efficiency and high peak power.